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Tensor Polarizabilities of Magnetoelectric Particles on the Base of Strip-Line-Coupled Magnetostatic Wave Resonators

S. V. Zagriadski

Radiophysics Department, St. Petersburg State Technical University
Polytekhnicheskaya 29, St. Petersburg, 195251, Russia
Fax: (7-812) 247-20-88, E-mail: zagr@radio.stu.neva.ru

Abstract

An electrodynamic description of bianisotropic particles on the base of strip-line-coupled magnetostatic wave (MSW) resonators is developed and analytical closed-form expressions for their tensor polarizabilities are obtained for an arbitrary direction of a magnetizing field and an arbitrary resonator shape. Numerical calculations are performed for a normally magnetized thin-ferrite-film disk resonator with a metal strip on its surface.

1. Introduction

Recently proposed composite non-reciprocal bianisotropic materials [1] represent ensembles of magnetized thin-ferrite-film magnetostatic wave resonators with surface metallization. Induced electric and magnetic dipole moments \mathbf{p}_e and \mathbf{p}_m of such artificial particles are related to the external electric and magnetic fields as

$$\mathbf{p}_e = \tilde{\alpha}_{ee} \mathbf{E} + \tilde{\alpha}_{em} \mathbf{H}, \quad \mathbf{p}_m = \tilde{\alpha}_{me} \mathbf{E} + \tilde{\alpha}_{mm} \mathbf{H}, \quad (1)$$

where $\tilde{\alpha}_{ee}$, $\tilde{\alpha}_{em}$, $\tilde{\alpha}_{me}$ and $\tilde{\alpha}_{mm}$ are corresponding tensor polarizabilities. Although a nature and qualitative physical picture of magnetoelectric coupling in these elements is quite obvious and an experimental evidence of the effect has been obtained [2], the electrodynamic description of the

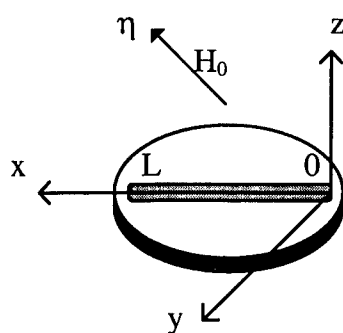


Fig. 1

particles and quantitative evaluation of magnetoelectric coupling till the present time has not been performed. In this paper we consider a thin-ferrite-film resonator with a linear metal strip of the width b on its surface, as shown in the Fig.1 for a disk resonator magnetized by the field H_0 in an arbitrary direction η . Dimensions of the resonator are much less than a wavelength in the surrounding media with the permittivity ϵ , so electric and magnetic fields in (1) can be assumed uniform and quasi-static. Magnetization of oscillation modes \mathbf{m}_q for the type q and corresponding eigenfrequencies ω_q are supposed to be known, as well the ferromagnetic resonance linewidths

ΔH_q . The approach is based on the earlier obtained solutions of self-consistent electrodynamic problems of the excitation of one-port [3] and two-port [4] MSW resonators. In this formulation, in particular, dipole moments of a particle, induced by an external magnetic field are found through a resonator high-frequency magnetization, which is determined taking into account the "back" influence of the current in the strip on this magnetization. Neglecting of this interaction results in the non-accurate determination of the polarizabilities $\tilde{\alpha}_{em}$, $\tilde{\alpha}_{mm}$ and their resonant frequency. Presented electrodynamic description of magnetoelectric particles enables to obtain constitutive relations for composite media in a closed form.

2. Self-Consistent Electrodynamic Problem for $\tilde{\alpha}_{em}$ and $\tilde{\alpha}_{mm}$ Determination

Tensor polarizabilities $\tilde{\alpha}_{em}$ and $\tilde{\alpha}_{mm}$ are calculated in the assumption that $\mathbf{E} = 0$ in (1). Magnetization induced by a given magnetic field \mathbf{H} is found as an expansion into the series of eigenmodes

$$\mathbf{M} = \sum_q c_q \mathbf{m}_q, \quad c_q = \varphi_q \int_V (\mathbf{H} + \mathbf{h}_\mu) \cdot \mathbf{m}_q^* dV, \quad (2)$$

where
$$\varphi_q = -\frac{b_q}{\omega^2 - \omega_q^2 - i\omega_q^2 Q_q^{-1}}, \quad b_q = \frac{i(\omega + \omega_q)\omega_M}{\Phi_q}, \quad \Phi_q = \int_V [\mathbf{m}_q \times \mathbf{m}_q^*]_\eta dV,$$

$$Q_q = \frac{H_0}{2\Delta H_q}, \quad \omega_M = \gamma\mu_0 M_0, \quad \gamma \text{ is the gyromagnetic ratio, } \mu_0 \text{ is the permeability of free space, } M_0$$

is the saturation magnetization, and V is the resonator volume. The "back" influence of a strip current on the magnetization is taken into account by including the magnetic field \mathbf{h}_μ in (2), which can be found as a field of a transmission line excited by an equivalent given magnetic current $i\omega\mathbf{M}$

$$\mathbf{h}_\mu = c_\mu(x)\mathbf{H}_\mu^r + c_{-\mu}(x)\mathbf{H}_{-\mu}^r, \quad (3)$$

with

$$c_\mu(x) = -\frac{i\omega\omega_0}{N_\mu^r} \int_0^x dx \int_S (\mathbf{M} \cdot \mathbf{H}_{-\mu}^r) dS, \quad c_{-\mu}(x) = -\frac{i\omega\omega_0}{N_\mu^r} \int_x^L dx \int_S (\mathbf{M} \cdot \mathbf{H}_{-\mu}^r) dS$$

where $\mathbf{H}_\mu^r = \mathbf{H}_\mu + \Gamma_2 \mathbf{H}_{-\mu}$, $\mathbf{H}_{-\mu}^r = \mathbf{H}_{-\mu} + \Gamma_1 \mathbf{H}_\mu$, $N_\mu^r = (1 - \Gamma_1 \Gamma_2) N_\mu$, $\mathbf{H}_{\pm\mu} = \mathbf{H}_{\pm\mu 0}(y, z) \exp(\mp i\beta x)$ is the magnetic field of a dominant wave in a strip-line (in the absence of ferrite) with the propagation constant β , N_μ is a normalization coefficient [4], Γ_1 and Γ_2 are the reflection coefficients for a strip current at $x = 0$ and $x = L$ ($\Gamma_1 = -1$ and $\Gamma_2 = -\exp(-2i\beta L)$ for our case of an open transmission line), and S is the cross section of the line. The system of integral equations (2), (3), formulating a self-consistent electrodynamic problem, has the following solution for amplitudes of electromagnetic waves in the transmission line

$$c_\mu(x) = \left[(e^{i\beta x} - 1) - \Gamma_1 (e^{-i\beta x} - 1) \right] c_{\mu 0}, \quad c_{-\mu}(x) = \left[(e^{-i\beta x} - e^{-i\beta L}) - \Gamma_1 (e^{i\beta x} - e^{i\beta L}) \right] c_{\mu 0}, \quad (4)$$

where
$$c_{\mu 0} = -\frac{i\omega\mu_0}{N_\mu} \left[i\beta(1 - \Gamma_1 \Gamma_2) + 2s \frac{i\omega\mu_0}{N_\mu} \varphi_q |I_{\mu q}|^2 \right]^{-1} I_{\mu q}^* \varphi_q \int_V (\mathbf{H} \cdot \mathbf{m}_q^*) dV, \quad I_{\mu q} = \int_S (\mathbf{H}_{\mu 0} \cdot \mathbf{m}_q^*) dS$$

and parameter s , depending on the line length, is given in [4] ($s \approx 2i\beta L^2$ for a special case $\beta L \ll 1$). Substituting (4) in (3) and using Ampere's law (an integration extends over an arbitrary contour C in the cross section yz which includes the strip)

$$\oint_C \mathbf{h}_\mu d\mathbf{l} = J(x),$$

one can find an induced electric dipole moment and using (2) - a magnetic dipole moment

$$\mathbf{p}_e = \frac{1}{i\omega} \mathbf{e}_x \int_0^L J(x) dx, \quad \mathbf{p}_m = \sum_q c_q \int_V \mathbf{m}_q dV. \quad (5)$$

Polarizabilities can be written in a tensor form

$$\tilde{\alpha}_{em} = A \cdot \begin{bmatrix} m_{qx}^* & m_{qy}^* & m_{qz}^* \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad \tilde{\alpha}_{mm} = B \cdot \begin{bmatrix} m_{qx} m_{qx}^* & m_{qx} m_{qy}^* & m_{qx} m_{qz}^* \\ m_{yx} m_{qx}^* & m_{qy} m_{qy}^* & m_{qy} m_{qz}^* \\ m_{qz} m_{qx}^* & m_{qz} m_{qy}^* & m_{qz} m_{qz}^* \end{bmatrix}, \quad (6)$$

where for the case $\beta L \ll 1$ coefficients A and B are the following

$$A = \frac{i}{6} \frac{\mu_0}{\sqrt{2WN_\mu}} \varphi_q I_{\mu q}^* V \beta^2 L^3 \left(-\beta + L \frac{\omega \mu_0}{N_\mu} \varphi_q |I_{\mu q}|^2 \right)^{-1}, \quad (7)$$

$$B = \varphi_q V^2 + \varphi_q^2 V^2 |I_{\mu q}|^2 \frac{\omega \mu_0 \beta^3 L^4}{3N_\mu} \left[i\beta(1 - \Gamma_1 \Gamma_2) + 2s\varphi_q |I_{\mu q}|^2 \frac{i\omega \mu_0}{N_\mu} \right]^{-1}, \quad (8)$$

and W is a characteristic impedance of a transmission line, which can be calculated as [5]

$$W = \frac{120}{\sqrt{\epsilon}} \left(\ln \frac{2.2L}{b} - 1 \right). \quad (9)$$

For a normally magnetized ferrite disk and a fundamental uniform mode of magnetization (when its components can be assumed to be $m_{qx} = 1$, $m_{qy} = -i$, $m_{qz} = 0$) calculated polarizability coefficients A (7) are shown in the Fig.2. Note that in this case an internal biasing magnetic field is uniform. The diameter of the resonator is taken equal to the length of a strip and the particle is characterized by the following set of parameters: $L = 0.5\text{mm}$, $b = 20\mu\text{m}$, $4\pi M_0 = 1750\text{ Oe}$, $H_0 = 5320\text{ Oe}$, $2\Delta H_0 = 0.5\text{ Oe}$, $\epsilon = 10$.

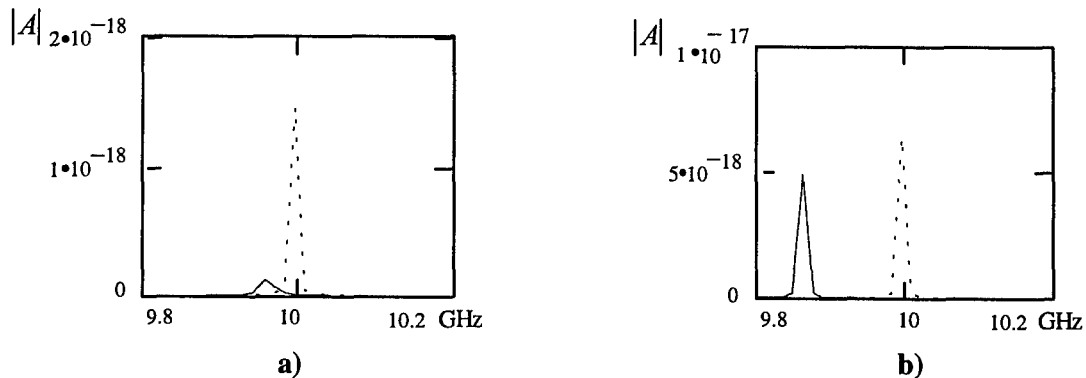


Fig. 2 Polarizability coefficient $|A|$ (ferrite film thickness: a) $10\mu\text{m}$, b) $50\mu\text{m}$). Solid curve: Self-consistent solution; Dotted: "Back" coupling neglected.

3. Calculation of Tensor Polarizabilities $\tilde{\alpha}_{ee}$ and $\tilde{\alpha}_{me}$

Tensor polarizabilities $\tilde{\alpha}_{ee}$ and $\tilde{\alpha}_{me}$ are calculated in the assumption that $\mathbf{H} = 0$ in (1). A current distribution along a narrow strip in an external longitudinal electric field \mathbf{E} is known from the antenna theory [5]

$$J(x) = J(L/2)f(x), \quad (10)$$

where $J(L/2) = \frac{2iE}{\beta W \cos(\beta L/2)} \left(1 - \cos \frac{\beta L}{2} \right)$, $f(x) = \frac{\cos \beta(x - L/2) - \cos(\beta L/2)}{1 - \cos(\beta L/2)}$. Induced electric dipole moment \mathbf{p}_e is obtained by integrating the current $J(x)$ according (5). A magnetic dipole moment

\mathbf{p}_m of the ferrite resonator is excited by the current (10) and can be calculated using (5) with the amplitude coefficients c_q being obtained from (2) for $\mathbf{H} = 0$. It can be easily seen that the magnetic field of the transmission line is related to the current as

$$\mathbf{h}_\mu = \frac{J(x)}{J_c} \mathbf{H}_{\mu 0}, \quad (11)$$

where $J_c = \oint_C \mathbf{H}_{\mu 0} d\mathbf{l}$ (for this value the following relationship is valid $J_c = \sqrt{N_\mu / (2W)}$).

Performing calculations we come to the following polarizabilities for the case $\beta L \ll 1$

$$\tilde{\alpha}_{ee} = C \cdot \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad \tilde{\alpha}_{me} = D \cdot \begin{bmatrix} m_{qx} & 0 & 0 \\ m_{qy} & 0 & 0 \\ m_{qz} & 0 & 0 \end{bmatrix}, \quad (12)$$

$$\text{where } C = \frac{1}{6} \frac{\beta L^3}{\omega W}, \quad D = \frac{i\beta L^3}{6W} \frac{\varphi_q I_{\mu q} V}{J_c}.$$

4. Conclusion

Derived explicit expressions for polarizabilities show that all non-zero tensor elements, except $\tilde{\alpha}_{ee}$, have resonant character with resonance frequencies close, but not equal, to the MSW resonator eigenfrequencies. Elements of tensors of magnetoelectric coupling $\tilde{\alpha}_{em}$, $\tilde{\alpha}_{me}$ are proportional to the saturation magnetization M_0 of ferrite and to the third power of the strip length L^3 and increase with the growth of the resonator quality factor Q . For low magnetic losses these tensors are related as $\tilde{\alpha}_{em} \approx \mu_0 \tilde{\alpha}_{me}^*$. Elements of the tensor $\tilde{\alpha}_{mm}$ are proportional to the resonator volume V . The tensor $\tilde{\alpha}_{ee}$ has no frequency dependence and is proportional to the third power of the strip length L^3 . In the case when a ferrite resonator has a non-elliptic form (e.g., a straight-edge MSW resonator with a film of a rectangular form), calculations of polarizabilities must be carried out taking into account the influence of nonuniformity of the internal biasing magnetic field [6].

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